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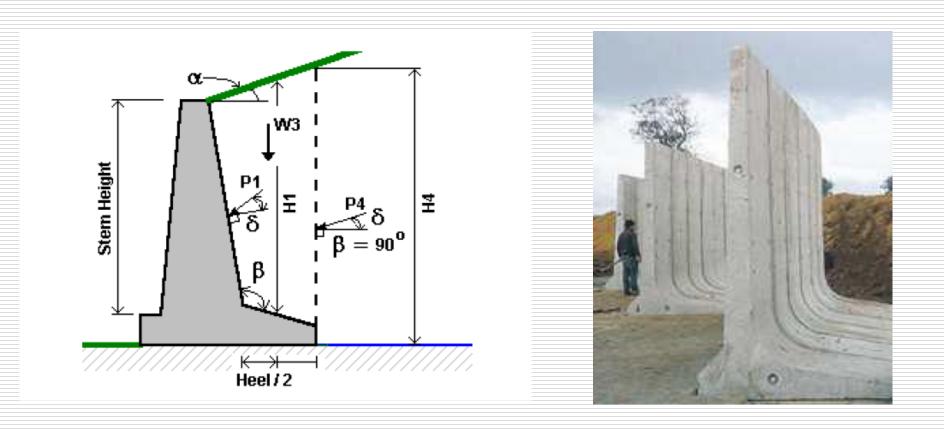
- CURS 6 -

Lateral Earth Pressure and Retaining Walls

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CHAPTER V – LATERAL EARTH PRESSURE AND RETAINING WALLS

□ A **retaining wall** is a wall that provides lateral support for a vertical or near vertical slope of soil.



CHAPTER V – LATERAL EARTH PRESSURE AND RETAINING WALLS

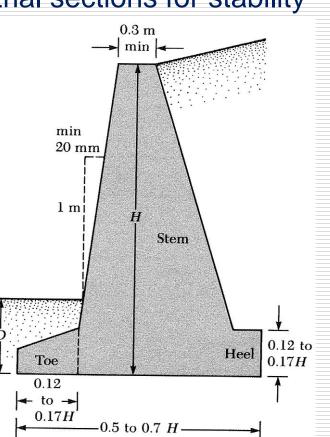
§ 5.3 Proportioning of retaining walls

□ When designing retaining walls, one must assume some of its dimensions (*proportioning*).

Proportioning allows the engineer to check trial sections for stability in an iterative process.

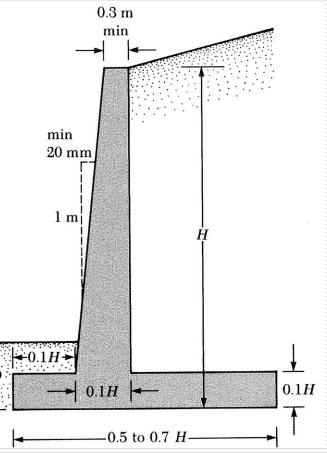
□ For gravity RW:

- **Top:** min 0.3m
- □ Sole length: 0.5-0.7H
- Heel height: 0.12-0.17 H
- □ Toe length: 0.12-0.17 H
- Frost depth (D): in accordance with the local frost conditions (not less than 0.6m)



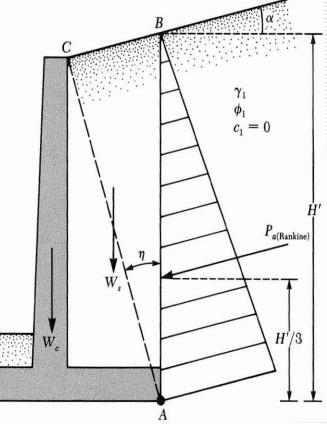
§ 5.3 Proportioning of retaining walls





§ 5.4 Design of retaining walls Application of Lateral Earth Pressure to Design

- □ For the design of RW, the general theories of application of lateral earth pressure on RW should be made on the basis of some assumptions:
- □ In case of cantilever RW, if the Rankine's earth pressure is to be used, then:
 - The active pressure is considered as acting on the vertical line starting from the edge of the heel.
 - □ The Rankine active pressure acts on the line AB, constructed from the heel edge.
 - The weight of the wall slabs and the weight of the soil above the heel acts on their centroids.
 - The weight of the wall slabs and the weight of the soil above the heel acts on their mid-widths.

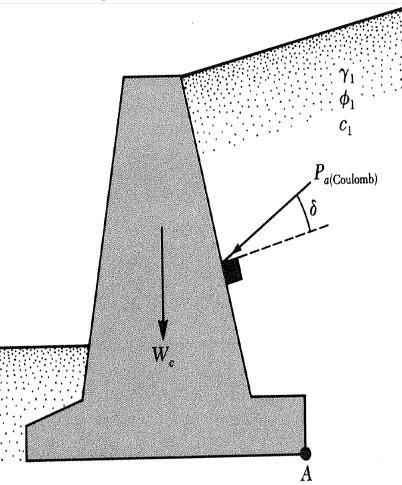


§ 5.4 Design of retaining walls Stability checks for retaining walls

Assumptions to check the stability of retaining walls in case of applying the Coulomb's theory:

- □ The forces to be considered are the active force P_a and the RW weight W_c
- The active pressure is considered as acting on the internal face of the wall.
- The angle δ made with the normal on the wall edge represents the friction angle between the soil and the retaining surface:

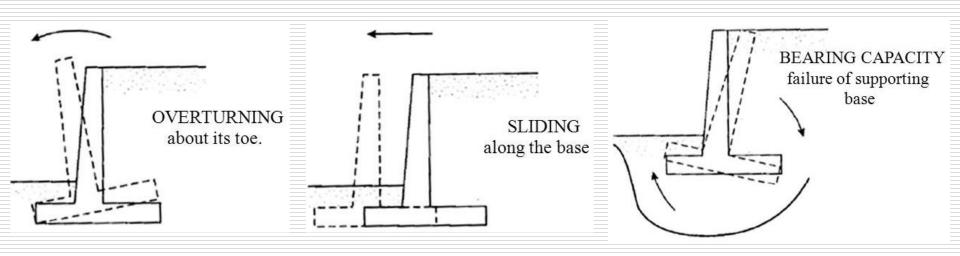
 $\delta = (1/2....1/3)\Phi$



 $\phi_2 \\ c_2$

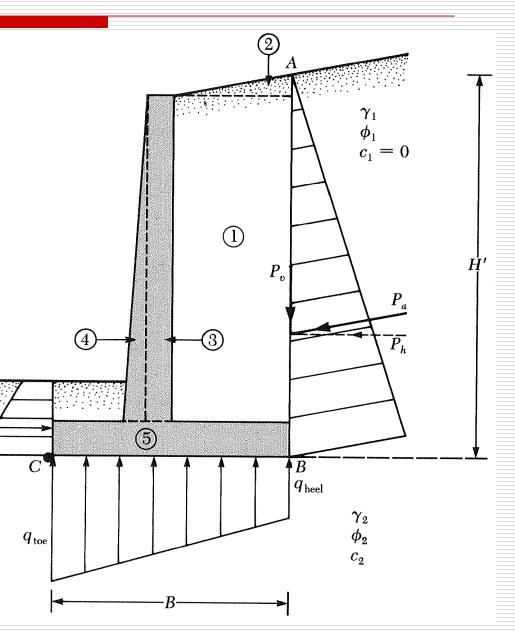
§ 5.4 Design of retaining walls Stability checks for retaining walls

- □ To check the stability of retaining walls, the following checks are necessary:
 - Check for overturning about toe
 - Check for sliding along its base
 - Check for bearing capacity failure at the base
 - Check for settlement
 - Check for overall stability



- □ The figure shows the forces acting on a cantilever (gravity) retaining wall.
- □ The Rankine Active Pressure P_a acts on the vertical plane AB drawn from the heel.
- □ On the same principles, the Rankine Passive Pressure P_p acts on the vertical plane C drawn from the toe.

$$P_p = \frac{1}{2} \cdot K_p \gamma_2 \cdot D^2 + 2c \cdot H \cdot \sqrt{K_p}$$



□ The factor of safety against overturning about point C is given as:

 $FS = \frac{\Sigma M_R}{\Sigma M_o}$

where:

 ΣM_R - sum of moments of forces tending to resist overturning about point C

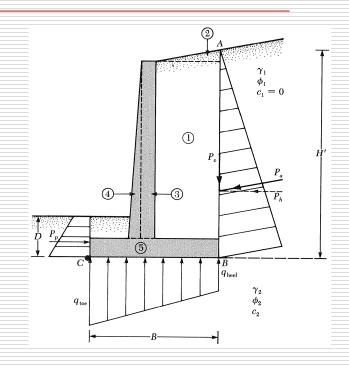
 ΣM_o - sum of moments of forces tending to overturn about point C

 $P_h = P_a \cdot \cos \alpha$ $\Sigma M_o = P_h \cdot H/3$

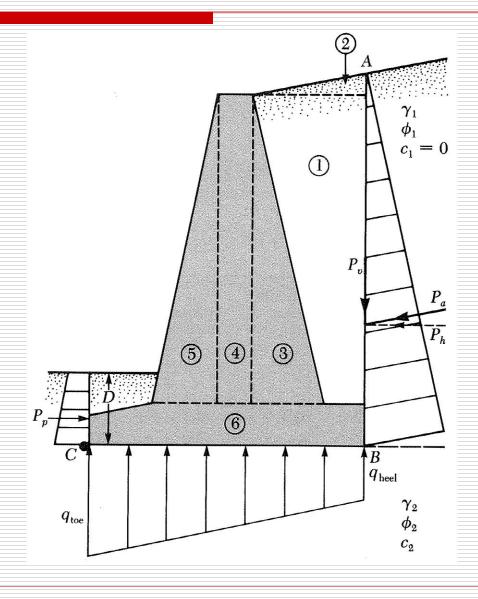
 $P_v = P_a \cdot \sin \alpha$ $\Sigma M_R = \Sigma W \cdot d + P_v \cdot B + P_p \cdot d_p$

□ The design should be repeated for each action combination (see C1)

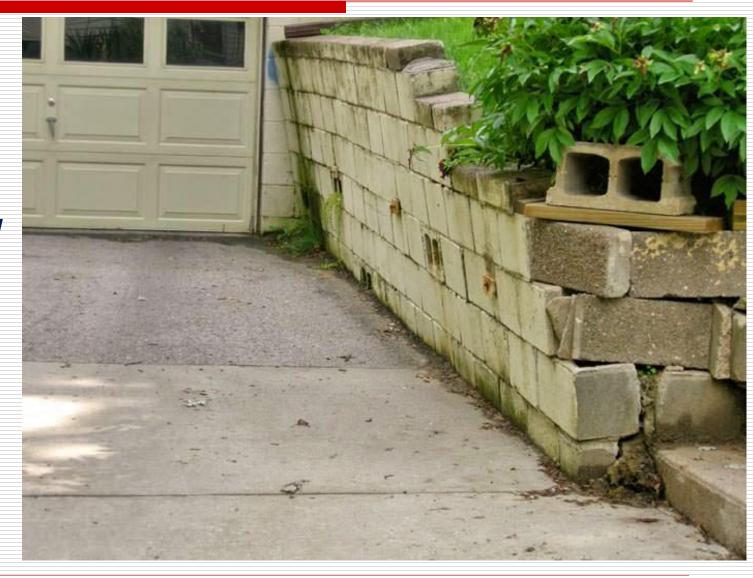
Obs: The usual minimum desirable values for the factor of safety with respect to overturning is 1.5...2.

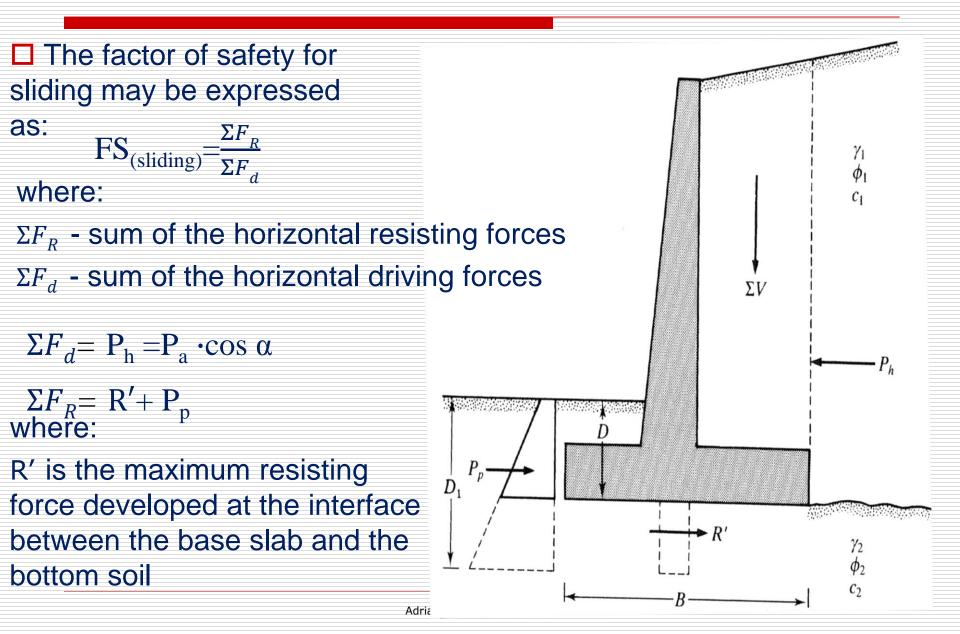


Check of overturning of gravity RW



Failure of RW by overturning:





§ 5.4 Design of retaining walls Stability checks for retaining walls – check for sliding $R'=\tau \cdot B = B \cdot (\sigma \cdot tan\Phi_2 + c_2) = B \cdot \sigma \cdot tan\Phi_2 + B \cdot c_2$ but: $B \cdot \sigma = \Sigma V$ - sum of the vertical forces

 $\frac{\gamma_2}{\phi_2}$

It results:

$$\Sigma F_R = (\Sigma V) \cdot \tan \Phi_2 + \mathbf{B} \cdot \mathbf{c}_2 + \mathbf{P}_r$$

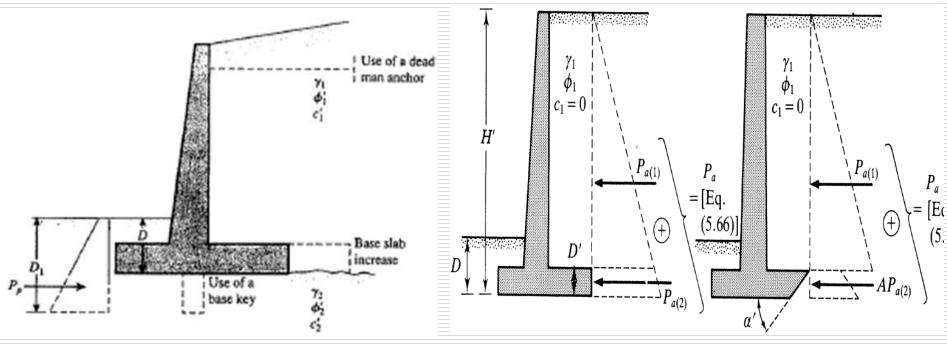
In consequence, the factor of safety for sliding may be expressed as:

$$FS_{(sliding)} = \frac{(\Sigma V) \cdot tan\Phi_2 + B \cdot c_2 + Pp}{P_a \cdot \cos \alpha}$$

Obs: The usual minimum desirable values for the factor of safety with respect to overturning is 1.0 in accordance to EN 1997-1, as the partial safety factors were included in the design combination of actions.

Obs 2: In many cases, the passive force P_p is ignored in calculation.

□ In many cases, the checking for sliding is not fulfilled. In order to improve the stability to sliding, we can adopt one of the following:



Use of a base key: this will generate an additional passive pressure (resisting force) on the key height; Modification of the shape of the supporting surface (reducing the active pressure on the base slab);

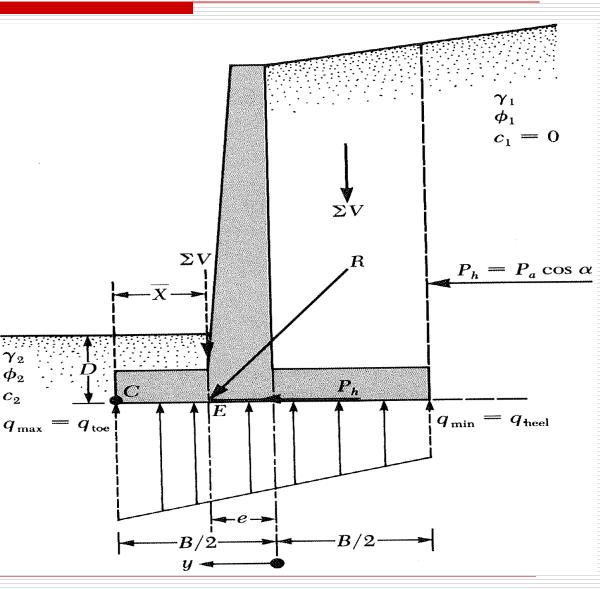
Failure of RW by sliding:



§ 5.4 Design of retaining walls Stability checks for RW – check for bearing capacity failure

□ The vertical pressure as transmitted to the soil by the base slab of the RW should be checked against the ultimate bearing capacity of the soil.

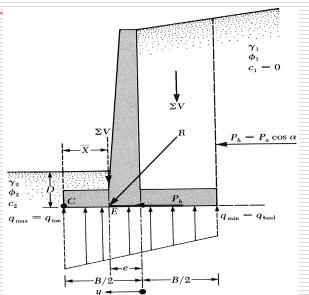
 \Box q_{toe} and q_{heel} represents the maximum and the minimum pressures occurring at the limits of the toe and heel sections.



§ 5.4 Design of retaining walls Stability checks for RW – check for bearing capacity failure

 \Box The values of q_{toe} and q_{heel} can be determined in the following manner:

- All the loads are reduced in a point on the basis of the foundation (e.g. center);
- There could be computed the sum of vertical forces: $V = \Sigma W_i + Pav$



The net moment of the foundation is: $M_{net} = \Sigma M_R - \Sigma M_Q$

 $\Box \text{ The values of } q(\sigma) \text{ results from: } q_{max/min} = \frac{V}{A} \pm \frac{M_{net}}{W} = \frac{V}{B \cdot 1} \pm \frac{M_{net}}{B^2 \cdot 1/6}$



Checking of the bearing capacity failure implies:

$$q_{max} \le q_{conv}$$

Obs: Usually the entire base slab should be in compression.

§ 5.4 Design of retaining walls Stability checks for RW – check for bearing capacity failure

Failure of RW by overpassing the bearing capacity:



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