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Title :

NUMERICAL MODELING OF REINFORCED CONCRETE COLUMNS STRENGTHENED WITH COMPOSITE MATERIALS

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Presented by :

Mr. C. OUCIF

SUMMARY

- Abstract.
- Geometry of the column.
- Materials properties.
- Experimental tests.
- Numerical modeling using ATENA software 2D.
- Results.
- Conclusion.

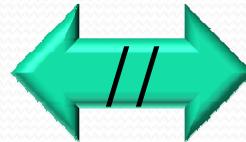
1. ABSTRACT

NUMERICAL MODELS



**BEHAVIOR UNDER CYCLIC
LOADING**

**Experimental RC columns
strengthened with
composite materials**



**Modeled RC columns
strengthened with
composite materials**

**STRENGTHENING
MATERIALS USED**

**Glass Fiber Reinforced
Polymers (GFRP)**

**BARS METALLIC
(BM)**

2. GEOMETRY OF THE COLUMN

Square cross section

Area of the column

• 25x25 cm²

Height of the column

• 150 cm

**Diameters of the
steel bars**

• 8, 10, 12 and 16 mm

2. GEOMETRY OF THE COLUMN

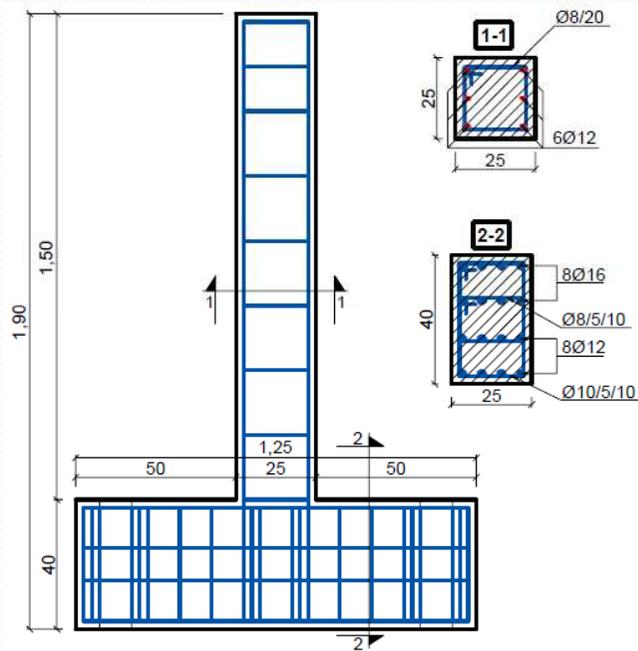


Figure 2.2 : Bars deformed [1].

Bars deformed before test

3. MATERIALS PROPERTIES

CONCRETE C16/20

**Compressive strength
[MPa]**

- $f_{ck,cube} = 27,5 \text{ MPa}$

**Elastic modulus
[MPa]**

- $E_c = 34500 \text{ MPa}$

**Tensile strength
[MPa]**

- $F_t = 2,187 \text{ MPa}$

3. MATERIALS PROPERTIES

Steel bars $\emptyset 8$, $\emptyset 10$, $\emptyset 12$, $\emptyset 16$

**Tensile strength
[MPa]**

• $f_t = 560 \text{ MPa}$

**Elastic modulus
[MPa]**

• $E_s = 200000 \text{ MPa}$

**Density
[Kg/m³]**

• $P = 7850 \text{ Kg/m}^3$

3. MATERIALS PROPERTIES

Glass Fiber Reinforced Polymers (GFRP)

Tensile strength
[MPa]

- $f_t = 2250 \text{ MPa}$

Elastic modulus
[MPa]

- $E = 70000 \text{ MPa}$

Density
[Kg/m³]

- $P = 2530 \text{ Kg/m}^3$

Thickness
[mm]

- $\varnothing = 0.17 \text{ mm}$

4. EXPERIMENTAL TESTS

13 attempts was performed
under cyclic loading [1]

For this article we study 02
attempts under cyclic loading
BM - GW

Hydraulic pump

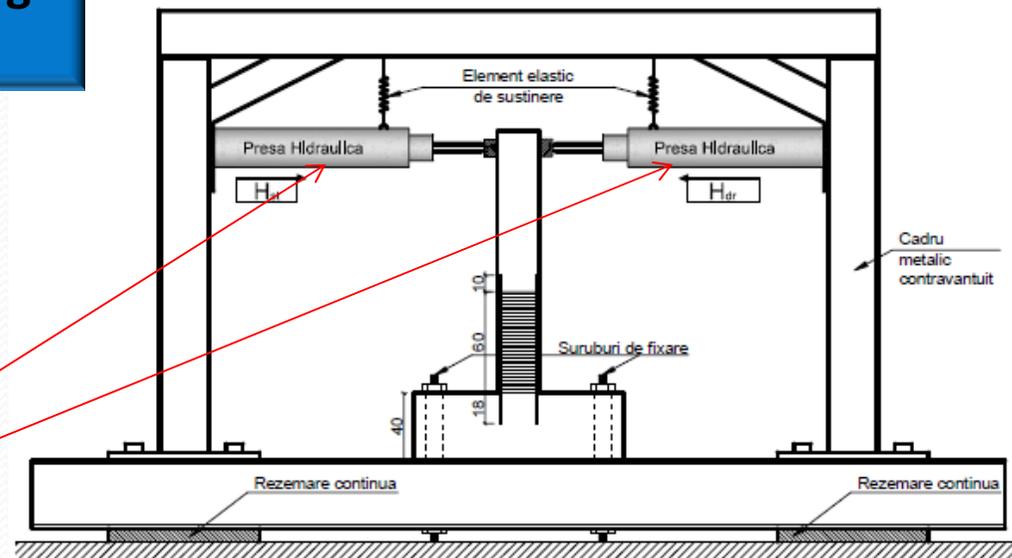


Figure 4.1 : Elements of the test bench [1].

4. EXPERIMENTAL TESTS

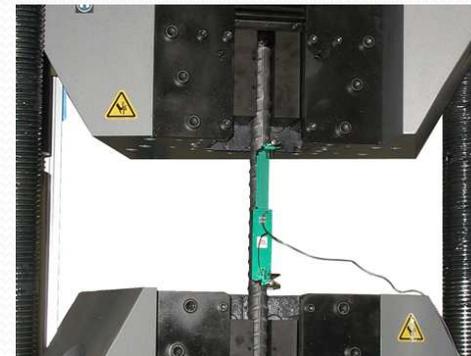
**Determination of the
limit of elastic behavior
25 kN – 24 mm**



Figure 4.2 : Reference model C1C [1].



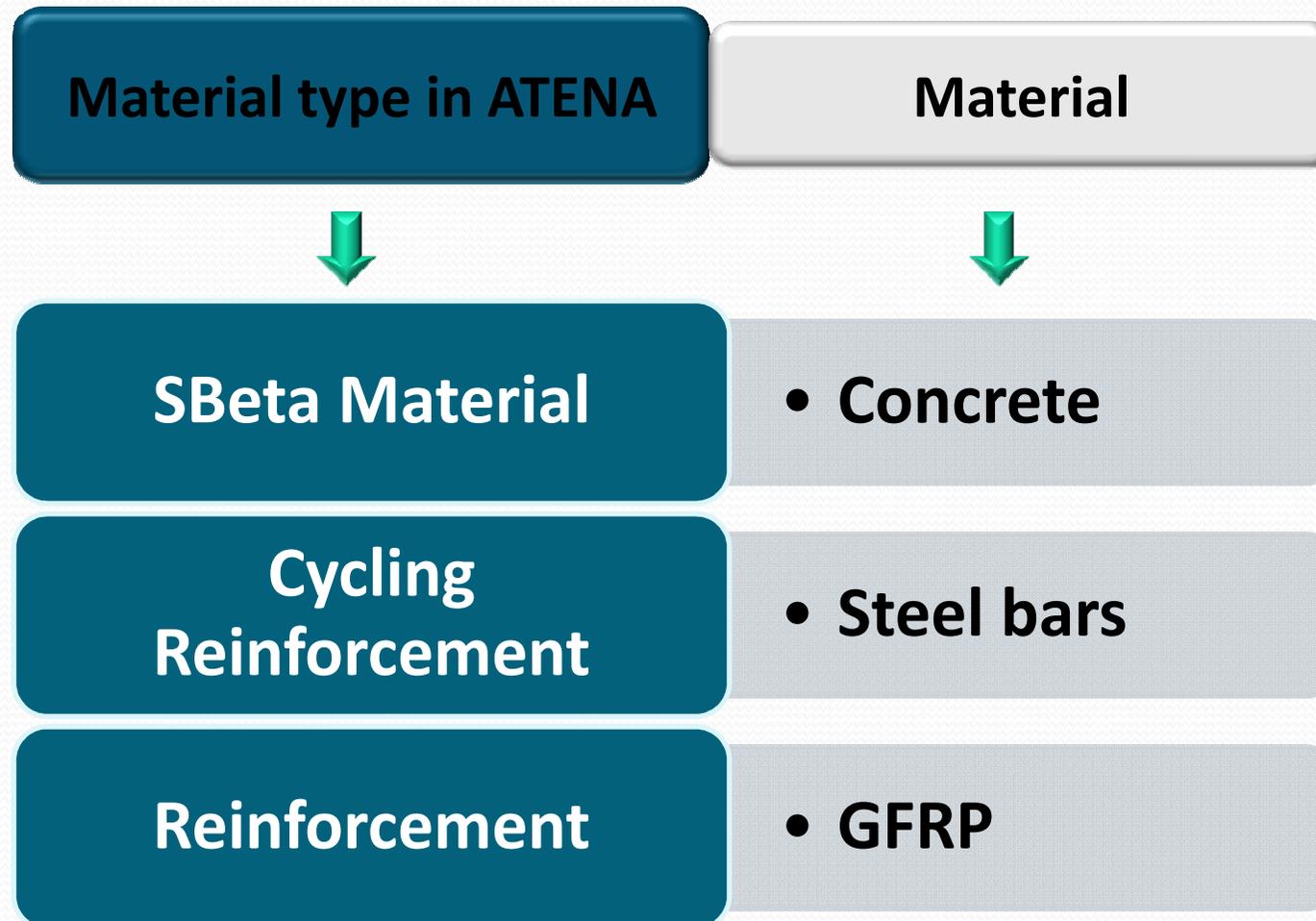
**Compression test on
concrete**



**Tensile test on
steel bars**

5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

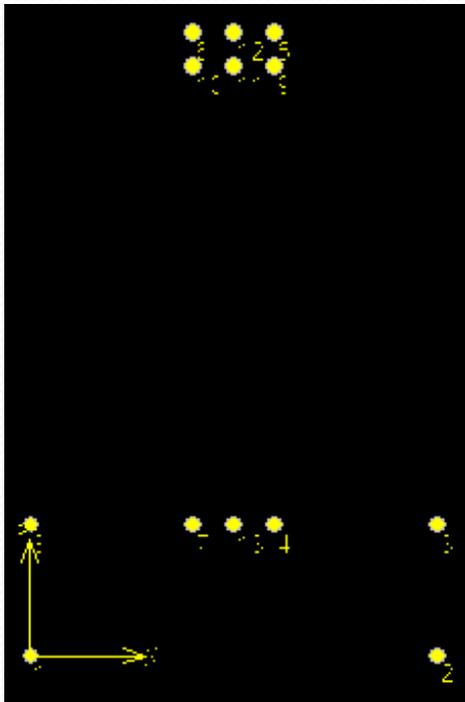
5.1. Definition of the materials



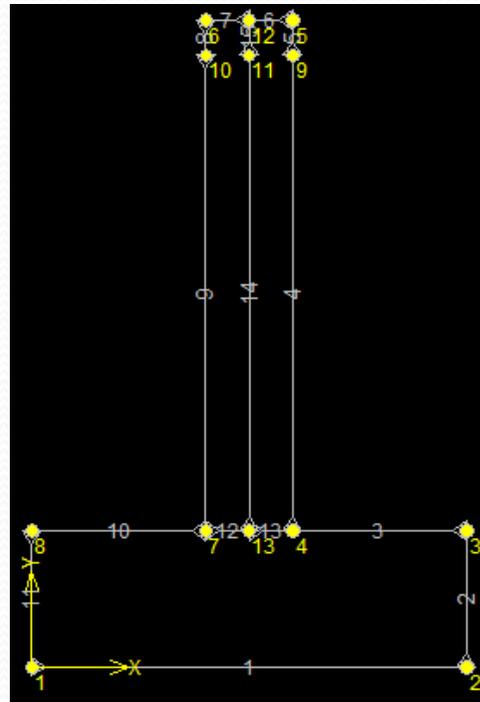
5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.2. Definition of the geometry

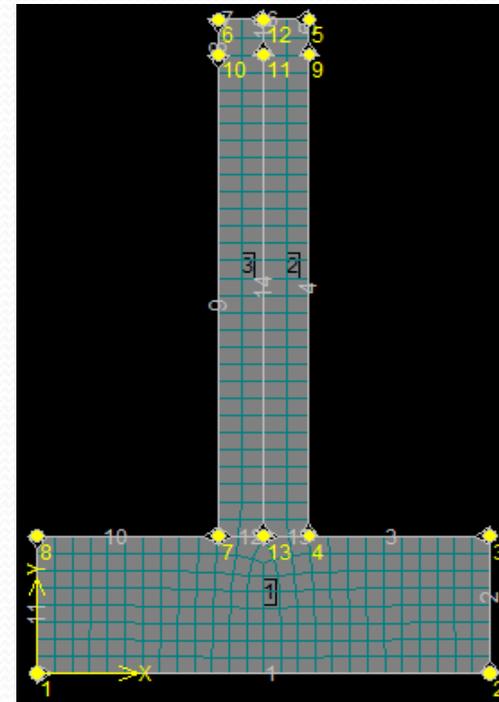
Joints



Lines



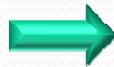
Macro-elements



5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.3. Definition of loading and support

Imposed
force



New load case

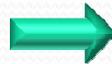
Load case
LC name: Load case with force
LC Code: Forces
LC coeff.: (konstantn) 1.0000 [-]

Dead load direction
X: 0.0000 [m] Y: -1.0000 [m]

LC number : 1

Add End

Imposed
displacement



New load case

Load case
LC name: Load case with displacement
LC Code: Prescribed deformatio
LC coeff.: (konstantn) 1.0000 [-]

Dead load direction
X: 0.0000 [m] Y: -1.0000 [m]

LC number : 1

Add End

5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.3. Definition of loading and support

Support



New load case

Load case

LC name: Support

LC Code: Supports

LC coeff.: (konstantni) 1.0000 [-]

Dead load direction

X: 0.0000 [m] Y: -1.0000 [m]

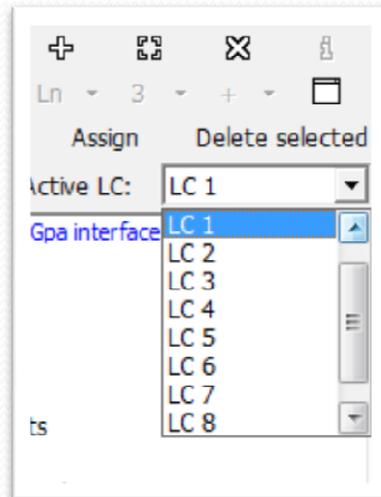
LC number : 1

Add End

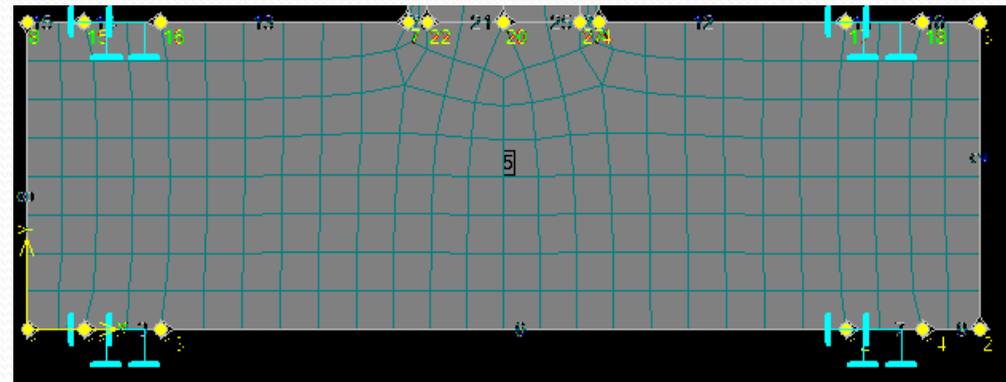
5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.4. Application of loading and support

Selection of the load case of support



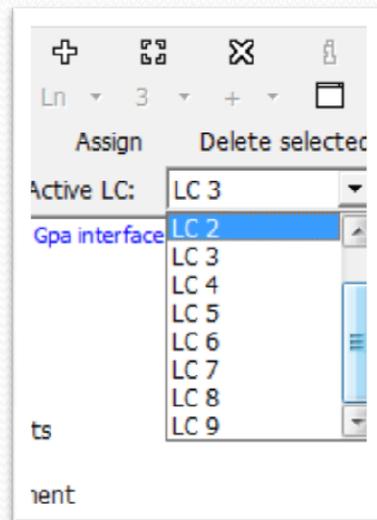
Application of the support



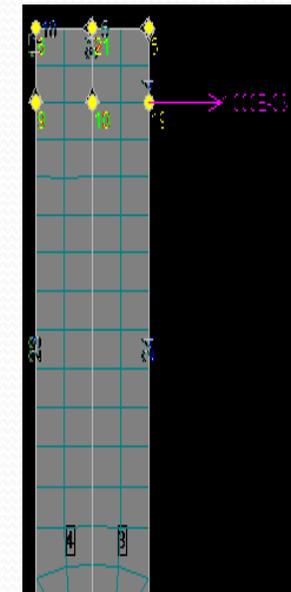
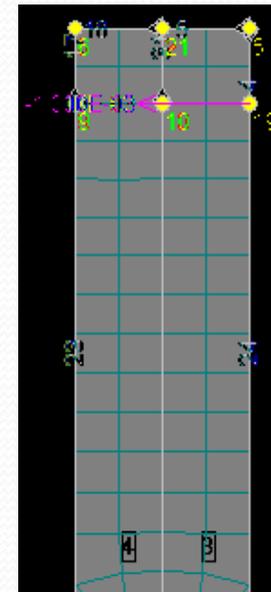
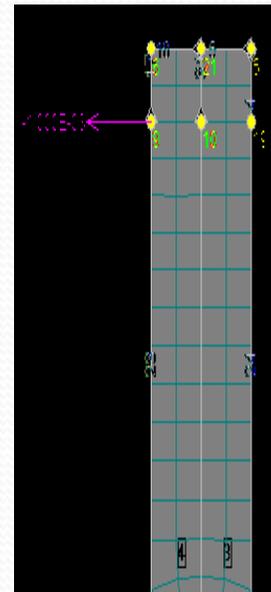
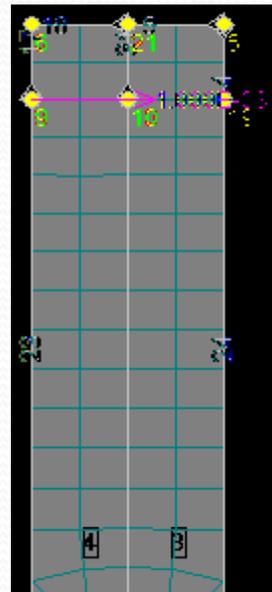
5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.4. Application of loading and support

Selection of the load case of loading



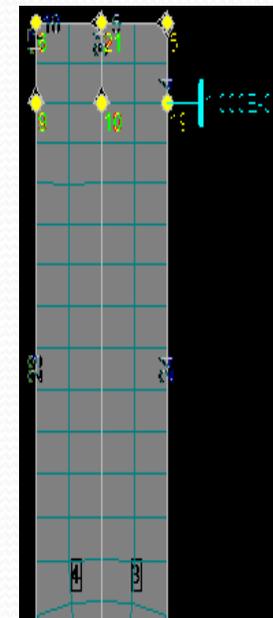
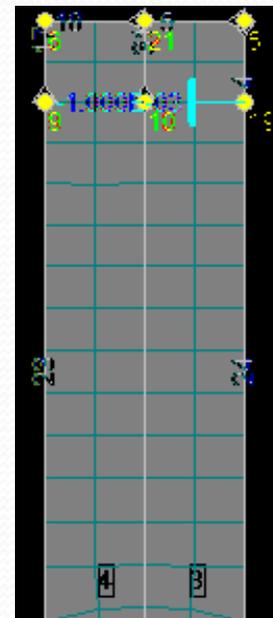
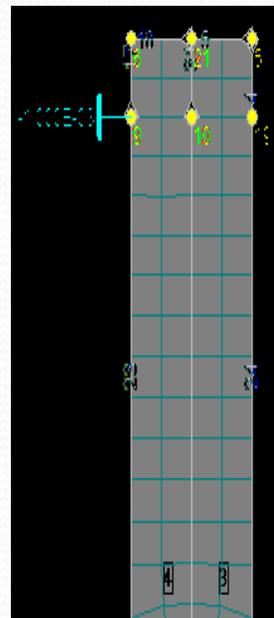
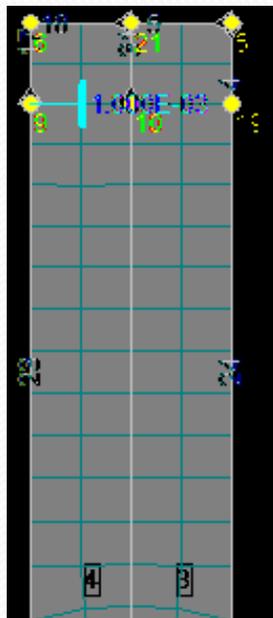
Application of the imposed forces (1 kN)



5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.4. Application of loading and support

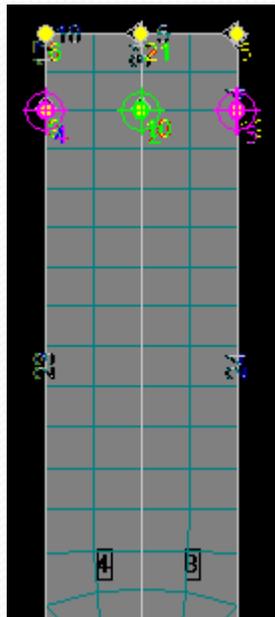
Application of the
imposed displacement
(1 mm)



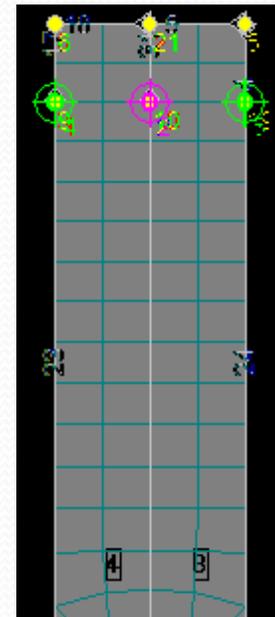
5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.5. Monitoring points

Control of displacement (D1)



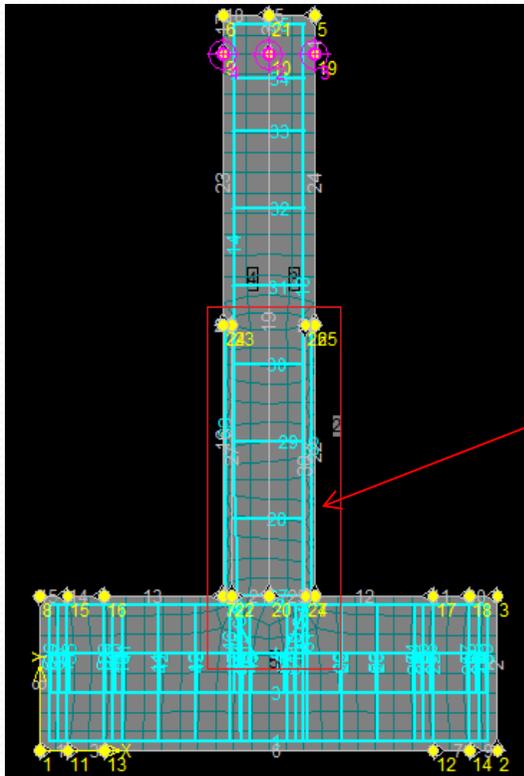
Control of force



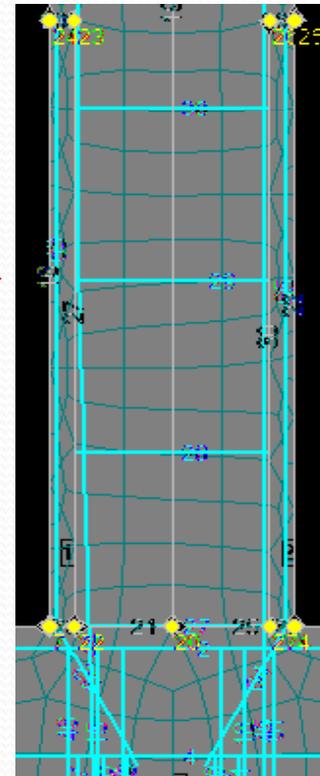
5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.6. Column strengthened with BM

Plan of the column
C3C-BM-AF



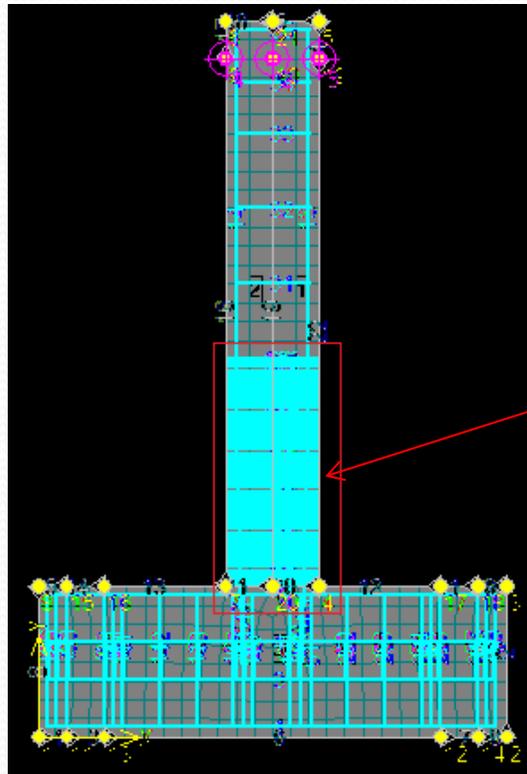
Detail of
strengthening



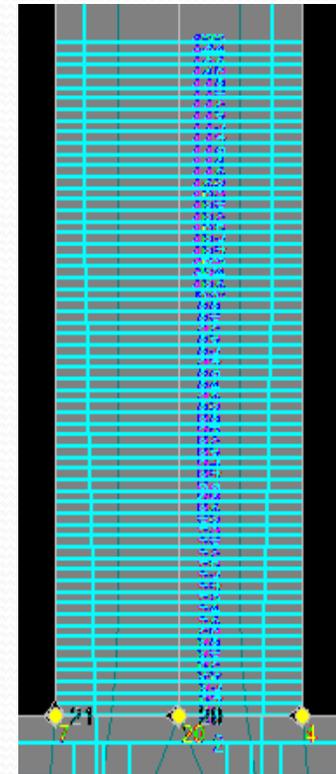
5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.7. Column strengthened with GFRP

Plan of the column
C6C1-GW-BC



Detail of
strengthening



5. NUMERICAL MODELING USING ATENA SOFTWARE 2D

5.8. Models used for materials

Concrete

- Non linear model for concrete.
- Strain softening in compression : softening law defined by means of the softening modulus.
- Strain softening in tension : Exponential crack opening law (Bazant 1983) [6].
- Rotated crack model for cracks.

Steel bars

- Perfect elastoplastic model.

GFRP

- Bilinear model.

6. RESULTS

6.1. C3C-BM-AF

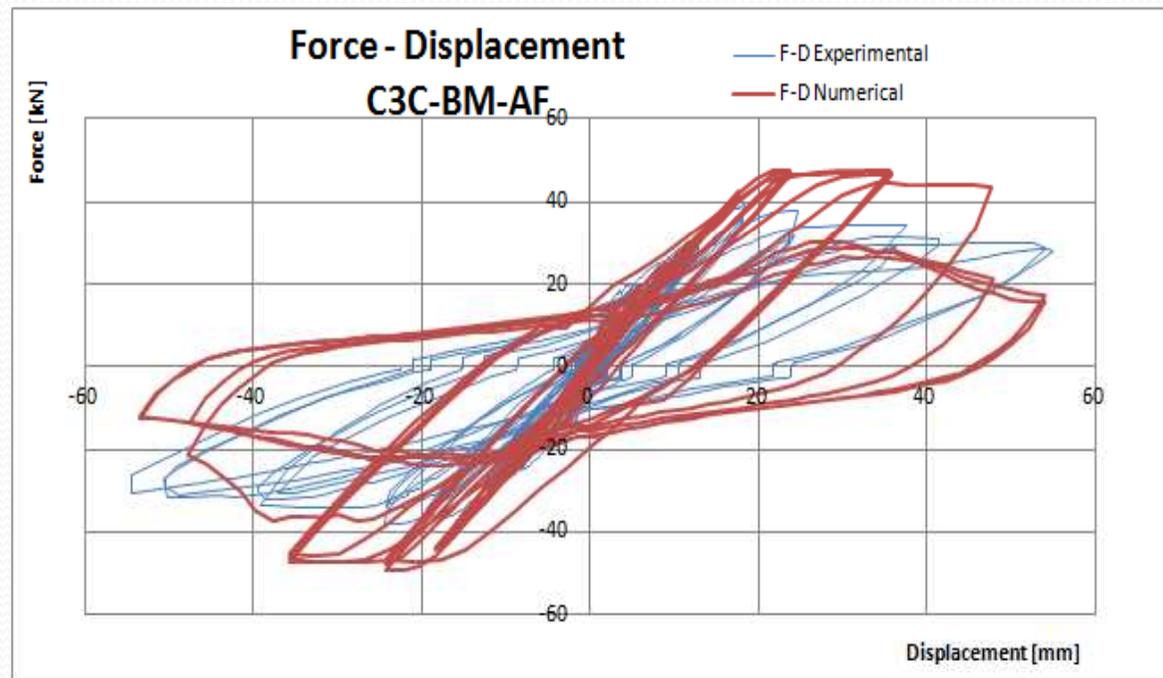


Figure 6.1 : Curve of comparison between the numerical and experimental test for the column C3C-BM-AF.

6. RESULTS

6.1. C3C-BM-AF

**Maximum
load**

Experimental : 38.15 kN

Numerical : 49.24 kN

**Maximum
displacement**

Experimental : 55.00 mm

Numerical : 54.04 mm



Figure 6.2 : Observed failure mechanism in experimental.

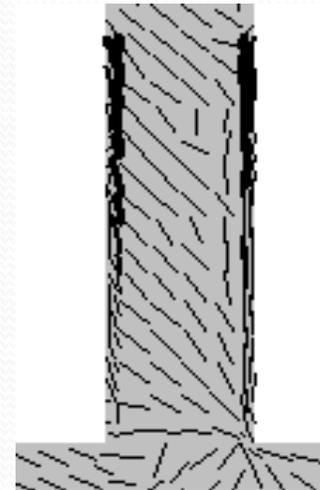


Figure 6.3 : Observed failure mechanism in numerical.

6. RESULTS

6.2. C6C1-GW-BC

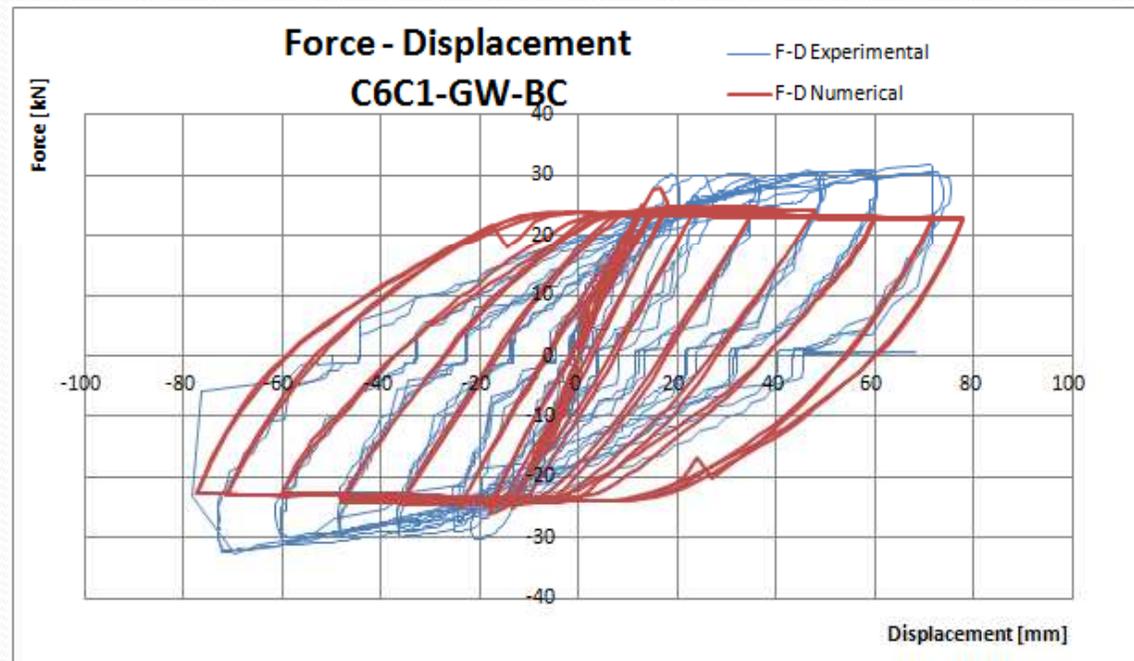


Figure 6.4 : Curve of comparison between the numerical and experimental test for the column C6C1-GW-BC.

6. RESULTS

6.2. C6C1-GW-BC

**Maximum
load**

Experimental : 32.83 kN

Numerical : 28.01 kN

**Maximum
displacement**

Experimental : 78.34 mm

Numerical : 77.82 mm



Figure 6.5 : Observed failure mechanism in experimental.

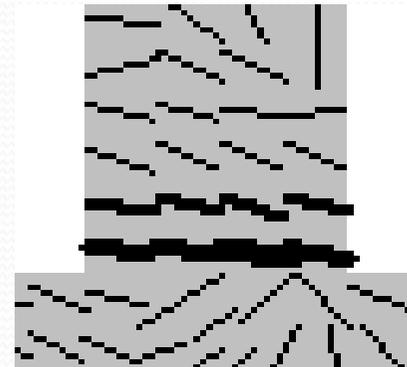


Figure 6.6 : Observed failure mechanism in numerical.

7. CONCLUSION

- Both numerical models for the columns strengthened with BM and GFRP show a behavior similar to the experimentally tested ones.
- **For C3C-BM-AF** : the numerical model is slightly more rigid compared to the experimental one. This can be partially due to the difference of the concrete constitutive model in the ATENA modeling and in the experimental test.
- **For C6C1-GW-BC** : The numerical behavior of the column is similar to the behavior of the experimental tested one.

This gives confidence to the design engineers and researchers in using finite element modeling for evaluating the cyclic behavior of RC columns strengthened with different types of composite materials.

To describe the real behavior of concrete elements strengthened with composite materials it is necessary to take into account all the parameters which can influence their behavior (thermal conditions, initial state of concrete, contact surfaces, boundary conditions . . .etc). This point is a subject for a future work.

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- [1] DĂESCU Alexandru Cosmin « REABILITAREA ELEMENTELOR DE CONSTRUCȚIE UTILIZÂND MATERIALE COMPOZITE POLIMERICE », PhD Thesis, Politehnica University of Timisoara, 212, 2011.
- [2] C. Desprez, J. Mazars, P. Kotronis, P. Paultre « Damage model for FRP-confined concrete columns under cyclic loading », Engineering Structures, France, 519-531, 2013.
- [3] Vladimír Červenka and Jan Červenka « User's Manual for ATENA 2D », Prague, 140, March 2010
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- [5] FEMA 547 « Techniques for the Seismic Rehabilitation of Existing Buildings ». 2006.
- [6] Stéphane Morel « Comportement courbe-R et effet d'échelle dans la rupture quasifragile. Cas des structures entaillées. », 25e rencontres de l'AUGC, Bordeaux, 8, 2007.



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